PHASE EQUILIBRIA IN THE METHANOL-CYCLOHEXENE SYSTEM

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Received April 14th, 1976

The liquid-vapour equilibrium in the methanol-cyclohexene system at 740, 521.5, 340.5, and 231.8 Torr, the liquid-liquid solubility equilibrium curve and the temperature dependence of the saturated vapour pressure of cyclohexene were measured. The correlation of equilibrium data was performed for each data set separately by the Wilson and NRTL equations and simultaneously by a six-constant equation which expresses the composition and temperature dependence of the excess Gibbs free energy with satisfactory agreement between experimental and calculated data.

In relation to estimation of the possibility of isolation of nonaromatic compounds from the benzene fraction, the liquid-vapour equilibrium in the methanol-cyclohexene system was measured. Equilibrium data of this system do not also lose theoretical attractivity as they supplement appropriately measurements in n-alcohols-benzene and n-alcohols-cyclohexane systems, which display such a strong nonideal behaviour that they are on the verge of the thermodynamic stability. As it was found during the experiments that the system exhibits a limited solubility region in the liquid phase, its boundary was established by determining the solubility curve. Finally, the temperature dependence of the saturated vapour pressure of cyclohexene was measured, which is necessary for correlating the equilibrium data and which has not been available with sufficient accuracy in the literature.

EXPERIMENTAL

Preparation of Pure Substances

Methanol. A mixture of methanol, A. R. grade, and the Grignard reagent was refluxed. The main portion of methanol was added into the boiling mixture and all was further heated for about 5 hours. The dried product was rectified on a 60-plate bubble cap column at the reflux ratio of 1 : 4. Its density and refractive index $(d_4^2 = 0.7866; n_D^{20} = 1.3287)$ agreed well with literature data¹. The Fischer analysis showed the content of water lower than 0-0025 wt.%.

Cyclohexene. Cyclohexene was prepared by dehydration of cyclohexanol with concentrated H_2SO_4 . The product was distilled off from the reaction mixture, shaken with a solution of ferric sulphate to remove peroxides, dried with CaCl₂ and rectified on a column packed with stainless helices whose efficiency was about 100 theoretical plates at the reflux ratio of 1 : 2. The distillate,

which contained 0.009 wt.% H₂O, was mixed with a 20fold excess of CaH₂ with respect to present H₂O, the mixture was again rectified on the same column and the middle fraction was taken off at an 1 : 5 reflux into ampules sealed with butadiene rubber stoppers. About 1/10 of the ampule content was occupied by the Nalsit A4 molecular sieves which were preliminarily activated for 10 hours at 360°C and simultaneously rinsed with dried nitrogen. The measured values of physicochemical constants, n.b.p. 83-01°C and n_D^{20} 1·4467, agree well with literature data¹ (n.b.p. 83-2; 83-19°C and n_D^{20} 1·4467). The Fischer analysis showed 0·0019 wt.% H₂O.

Apparatus

The liquid-vapour equilibrium was measured on a Gillespie still as modified by Otsuki and Williams^{2,3}. The sampling of the vapour and liquid phases was by syringes from closures sealed with butadiene rubber packings. The pressure was adjusted and stabilized by a vacuum stand, which maintained the pressure in the equilibrium still with a 0·1 Torr accuracy. The temperature was measured by a platinum resistance thermometer, which was calibrated preliminarily at the triple point of water and at 14 values of pressure from the range between 47°C and 99°C in two parallelly connected equilibrium stills filled with redestilled water. The reference temperature was being determined by standard thermometers. Calibrating points obtained in this manner were smoothed by the least squares method using a quadratic interpolation. It may be assumed that this arrangement enables one to measure the temperature in the equilibrium cell of the recirculation still with an accuracy better than $\pm 0.02^{\circ}C$.

The saturated vapour pressure of cyclohexene was measured on a Swietoslawski ebulliometer⁴ connected to the same vaccum stand and the liquid-liquid equilibrium by the usual turbidity method.

Determination of the Composition of Equilibrium Mixtures

The composition of equilibrium mixtures was determined refractometrically. Since the equilibrium behaviour is extremely sensitive to the water content, the measurements had to be performed in a dry box. The measured values, which covered the whole concentration range, were smoothed by the least squares method using a third-order polynomial. The composition dependence of the refractive index of the mixture is expressed by the relation

$$n_{\rm D}^{20} = 1.4467 - 0.137970 \, w_1 + 0.024553 \, w_1^2 - 0.005065 \, w_1^3 \,, \tag{1}$$

where w_1 is the weight fraction of methanol in the mixture. The assumed accuracy of the determination is ± 0.2 wt.%.

RESULTS

Saturated vapour pressures of cyclohexene are in Table I. Their temperature dependence was correlated by the Antoine equation whose constants were determined by minimizing the sum of squared deviations.

Liquid-vapour equilibrium data are in Table II. They were correlated by minimizing deviations of the logarithm of the ratio of activity coefficients expressed through the van Laar, Margules, and Scatchard third-order equations⁵ and Wilson

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The Temperature Dependence of the Saturated Vapour Pressure of Cyclohexene

| t, °C | 16.39 | 19.65 | 22.31 | 25.08 | 27.35 | 30.90 | 34.86 | 39.22 |
|---------|-------|-------|-------|-------|-------|-------|-------|-------|
| P, Torr | 60.0 | 69.6 | 78.8 | 89.6 | 99.2 | 115.6 | 137-1 | 164.3 |
| t, °C | 42.78 | 47.91 | 53.12 | 58.35 | 64.66 | 70.95 | 77.67 | 82.10 |
| P, Torr | 189.8 | 231.8 | 283.8 | 340.5 | 423.1 | 521.5 | 644.6 | 739-4 |

TABLE II

Experimental Liquid-Vapour Equilibrium Data of the Methanol(1)-Cyclohexene(2) System

| <i>x</i> ₁ | y_1 | t, °C | <i>x</i> ₁ | <i>y</i> ₁ | t, °C |
|-----------------------|--------|---------|-----------------------|-----------------------|-------|
| | | P = 740 | 0·0 Torr | | |
| 0.0083 | 0.2677 | 72.14 | 0.4205 | 0.6064 | 55.52 |
| 0.0130 | 0.3247 | 69.80 | 0.4656 | 0.6098 | 55.47 |
| 0.0238 | 0.4093 | 65.84 | 0.5166 | 0.6127 | 55-39 |
| 0.0292 | 0.4488 | 63.79 | 0.5782 | 0.6163 | 55-36 |
| 0.0347 | 0.4901 | 61.62 | 0.6350 | 0.6188 | 55-35 |
| 0.0488 | 0.5215 | 59.97 | 0.6934 | 0.6238 | 55-35 |
| 0.0680 | 0-5454 | 58.53 | 0.7497 | 0.6318 | 55.36 |
| 0.0868 | 0.5604 | 57.67 | 0.7916 | 0.6414 | 55-44 |
| 0.1248 | 0.5774 | 56.78 | 0.8342 | 0.6554 | 55.78 |
| 0.1658 | 0.5868 | 56-25 | 0.8804 | 0.6847 | 56-36 |
| 0.2344 | 0.5950 | 55.81 | 0.9137 | 0.7216 | 57.27 |
| 0.2859 | 0.5992 | 55.63 | 0.9476 | 0.7849 | 58.84 |
| 0.3557 | 0.6022 | 55.55 | 0.9656 | 0.8364 | 59-96 |
| | | P = 52 | 1·2 Torr | | |
| 0.0184 | 0.4025 | 56.04 | 0.5764 | 0.5980 | 46.58 |
| 0.0275 | 0.4708 | 52.96 | 0.6245 | 0.6031 | 46.59 |
| 0.0400 | 0.5040 | 51.29 | 0.6854 | 0.6064 | 46.60 |
| 0.0576 | 0.5309 | 49.73 | 0.7338 | 0.6139 | 46.62 |
| 0.0985 | 0.5622 | 48.31 | 0.7638 | 0.6197 | 46.73 |
| 0.1199 | 0.5694 | 47.91 | 0.7999 | 0.6262 | 46.82 |
| 0.1886 | 0.5746 | 47.18 | 0.8489 | 0.6461 | 47.16 |
| 0.2366 | 0·5791 | 47.03 | 0.8854 | 0.6721 | 47.75 |
| 0.2978 | 0.5843 | 46.90 | 0.9178 | 0.7119 | 48.62 |
| 0.3335 | 0.5860 | 46.85 | 0.9424 | 0.7568 | 49.73 |
| 0.4195 | 0.5903 | 46.73 | 0.9660 | 0.8242 | 51.31 |
| 0.4871 | 0.5937 | 46.65 | 0.9836 | 0.9024 | 53-12 |

| TABLE II Continued) | | | | | |
|------------------------|-----------------------|--------|-----------------------|-----------------------|-------|
| . x ₁ | <i>y</i> ₁ | t, °C | <i>x</i> ₁ | <i>y</i> ₁ | t, °C |
| | | P = 34 | 0·0 Torr | | |
| 0.0184 | 0.4049 | 44.66 | 0.5808 | 0.5834 | 36.68 |
| 0.0275 | 0.4687 | 41.89 | 0.6310 | 0.5860 | 36.66 |
| 0.0400 | 0.5040 | 40.28 | 0.6920 | 0.5903 | 36.68 |
| 0.0594 | 0.5272 | 39.12 | 0.7378 | 0.5972 | 36.73 |
| 0.0985 | 0.5514 | 37.98 | 0.7689 | 0.6039 | 36.82 |
| 0.1117 | 0.5532 | 37.80 | 0.8029 | 0.6089 | 36.89 |
| 0.1673 | 0.5595 | 37.17 | 0.8526 | 0.6286 | 37.26 |
| 0.2209 | 0.5631 | 37.07 | 0.8889 | 0.6554 | 37.83 |
| 0.2859 | 0.5649 | 36.97 | 0.9197 | 0.6941 | 38.72 |
| 0.3247 | 0.5694 | 36.93 | 0.9450 | 0.7451 | 39.88 |
| 0.4128 | 0.5755 | 36.81 | 0.9680 | 0.8151 | 41.53 |
| 0.4871 | .0.5791 | 36.68 | | | |
| | | P = 23 | 0·5 Torr | | |
| 0.0166 | 0.3991 | 35.33 | 0.5860 | 0.5685 | 28.33 |
| 0.0220 | 0.4572 | 32.91 | 0.6350 | 0.5711 | 28.33 |
| 0.0382 | 0.4961 | 31.35 | 0.6963 | 0.5764 | 28.35 |
| 0.0282 | 0.5176 | 30.34 | 0.7411 | 0.5817 | 28.40 |
| 0.0952 | 0.5375 | 29.43 | 0.7739 | 0.5886 | 28.48 |
| 0.1082 | 0.5385 | 29.34 | 0.8064 | 0.5954 | 28.52 |
| 0.1765 | 0.5487 | 28.79 | 0.8553 | 0.6131 | 28.88 |
| 0.2237 | 0.5523 | 28.69 | 0.8918 | 0.6406 | 29.46 |
| 0.2819 | 0.5568 | 28.60 | 0.9233 | 0.6803 | 30.39 |
| 0.3335 | 0.5613 | 28.55 | 0.9476 | 0.7345 | 31.80 |
| 0.4150 | 0.5640 | 28.50 | 0.9692 | 0.8111 | 33.27 |
| 0.4951 | 0.5667 | 28.40 | | | |

1456

and NRTL equations with $\alpha = 0.47$ (ref.⁶). The natural logarithm of the ratio of activity coefficients of each component was calculated from the equation

$$\log \gamma_{i} = \ln \left(y_{i} P / x_{i} P_{i}^{0} \right) + \left[\left(B_{ii} - v_{i}^{L} \right) \left(P - P_{i}^{0} \right) + P \delta_{ij} y_{j}^{2} \right] / RT, \qquad (2)$$

in which $\delta_{ij} = 2B_{ij} - B_{ii} - B_{jj}$ $(j \neq i)$, the temperature dependence of molar liquid volumes was considered to be linear, and the second virial coefficients of both pure components as well as the second cross virial coefficient were calculated by the O'Connell and Prausnitz method⁷ with critical constants evaluated according to Kud-

Jůza, Svoboda, Holub, Pick:

chadker and coworkers.⁸. All values necessary for the calculation of activity coefficients including the constants in the Antoine equation are given in Table III. The results of the correlations are in Table IV. Since, according to our expectation, the correlations by equations derived from the Wohl third-order expansion yielded inappropriate results, the table contains only values calculated from the Wilson and NRTL equations. Simultaneously, the data sets were correlated by the following six-constant equation

$$G^{\rm E}/RT = \exp\left[\left(\alpha + bT\right)x_1\right]x_1x_2\left[A_0 + BT + A_1(x_1 - x_2) + A_2(x_1 - x_2)^2\right],$$
(3)

TABLE III Constants Necessary for the Calculation of the Activity Coefficient

| Constants in | | | | | | |
|----------------|-------------------------|--|--|---|--|---|
| A | В | С | Ref. | OA | OB | Ref. |
| 7.87863 | 1 473-11 | 230 | 10 | 24.16 | 0.05734 | 1 |
| 6.91415 | 1 249.01 | 226.656 | this work | 63.94 | 0.12731 | 1 |
| T _k | P _k | v _k | ω_{H} | μ | η | Ref. |
| 513-2 | 78.5 | 118.0 | 0.105 | 1.66 | 1.21 | 7,8 |
| 559-2 | 41.8 | 285.0 | 0.209 | 0.00 | 0.00 | 7,8 |
| | A 7·87863 6·91415 | A B 7.87863 1 473.11 6.91415 1 249.01 T_k P_k 513.2 78.5 | $\begin{array}{cccccccc} A & B & C \\ \hline 7.87863 & 1 & 473 \cdot 11 & 230 \\ 6.91415 & 1 & 249 \cdot 01 & 226 \cdot 656 \\ \hline T_k & P_k & v_k \\ 513 \cdot 2 & 78 \cdot 5 & 118 \cdot 0 \end{array}$ | $7\cdot 87863$ $1 \cdot 473 \cdot 11$ 230 10 $6 \cdot 91415$ $1 \cdot 249 \cdot 01$ $226 \cdot 656$ this work T_k P_k v_k ω_H $513 \cdot 2$ $78 \cdot 5$ $118 \cdot 0$ $0 \cdot 105$ | Constants in the Antoine equation dependen A B C Ref. OA 7.87863 1 473·11 230 10 24·16 6·91415 1 249·01 226·656 this work 63·94 T_k P_k v_k ω_H μ 513·2 78·5 118·0 0·105 1·66 | A B C Ref. OA OB 7.87863 1473-11 230 10 24·16 0·05734 6·91415 1 249·01 226·656 this work 63·94 0·12731 T_k P_k v_k ω_H μ η 513·2 78·5 118·0 0·105 1·66 1·21 |

TABLE IV

The Correlation of Separate Sets of Liquid-Vapour Equilibrium Data

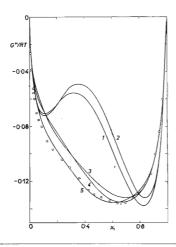
| Equation | P, Torr | Κ1 | К2 | $y^{exp} - y^{calc}$ |
|-----------------|---------|---------|---------|----------------------|
| Wilson | 740 | 2 315.4 | 488.6 | 0.0054 |
| | 521.2 | 2 385.4 | 476-7 | 0.0059 |
| | 340.0 | 2 364.1 | 524.9 | 0.0020 |
| | 230-5 | 2 397.6 | 531-1 | 0.0082 |
| NRTL | 740 | 1 637.6 | 1 183-7 | 0.0095 |
| $\alpha = 0.47$ | 521-2 | 1 664.5 | 1 171.5 | 0.0099 |
| | 340.0 | 1 662.4 | 1 208.0 | 0.0108 |
| | 230.5 | 1 692-4 | 1 212.8 | 0.0148 |

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which has been described in one of our earlier works⁹. With the following values of constants ($\alpha = -0.59315$, $\beta = 0.001$, $A_0 = 4.10423$, B = -0.00567, $A_1 = 0.49146$, $A_2 = 0.57303$), the computations yielded satisfactory agreement between measured and calculated values. (The difference in the mole fraction of methanol in the vapour phase for individual values of pressure (740, 521.5, 340.5, 231.8) was 0.0107, 0.0089, 0.0098, 0.0114, the difference in the calculated pressure in % 0.8, 1.2, 1.3, 0.9, and G^E calculated from experiments according to Eq. (3) 0.0028, 0.0023, 0.0023, 0.0023.

Values of the liquid-liquid solubility curve are in Table V.

| | TABLE V The Solubility Curve of the Methanol(1)–Cyclohexene(2) System | | | | | | | | | |
|-----------------------|--|--------|-------|------|-------|--------|--------|--------|--------|--|
| <i>x</i> ₁ | 0.10 | 0.17 | 0.205 | 0.26 | 0.315 | ,0.315 | 0.36 | 0.40 | 0.42 | |
| <i>ı</i> , °C | 13-15 | - 5.30 | 0.82 | 3.15 | 4.90 | 5.15 | 5.10 | 5-45 | 5.50 | |
| x2 | 0.44 | 0.50 | 0.56 | 0.60 | 0.64 | 0.68 | 0.73 | 0.81 | 0.92 | |
| t.°C | 5.60 | 5.40 | 5.05 | 4.25 | 3.05 | 1.30 | - 5.15 | -16.15 | -41.85 | |





The Dependence of G^M/RT on the Liquid Phase Composition at 740 Torr

• Experimental points, 1 van Laar, 2 Margules, 3 Wilson, 4 NRTL, 5 the six-constant equation.

DISCUSSION

The methanol-cyclohexene system is a highly nonideal one, which imposes extreme demands both on experimental technique and on the analytic evaluation of data. Above all, the equilibrium behaviour is extremely sensitive to the presence of water whose traces bring about the separation into two liquid phases up to the normal boiling point. Besides this, in the region of mole fractions of methanol of 0.1-0.7 the mixture possesses an extremely low surface tension and, consequently, necessary precautions had to be taken to avoid foaming of the mixture in the equilibrium cell.

Analogously, the correlation of the data is extremely difficult due to the exceptional course of the equilibrium curve. Correlation relations derived from the Wohl's third-order expansion exhibit an insufficient flexibility and can express this course only by an S-shaped curve which indicates a two-phase region and is of no physical meaning. Only the Wilson and NRTL equations are sufficiently flexible. For the latter equation it would still be possible to improve slightly the agreement by optimizing the constant a. Since, for more general purposes, it is more advantageous to compare correlation calculations using the same value of the constant α , we retained the value which was recommended by the author of the equation⁶ and which has been employed earlier for correlations in benzene-alcohol and cyclohexane-alcohol systems. The six-constant equation can then with good results express simultaneously both the temperature and concentration dependence. The situation is well illustrated on Fig. 1 which contains plots of the dependences of G^{M}/RT as they were calculated from individual correlation equations and experimental points and which may simultaneously serve as a document that the investigated system can become - due to its exceptional equilibrium behaviour - a good standard for testing the adequacy of employed correlation relations.

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Translated by K. Hlavatý.

Collection Czechoslov. Chem. Commun. [Vol. 42] [1977]